

Spatially Controllable CVD: The Programmable Reactor Concept

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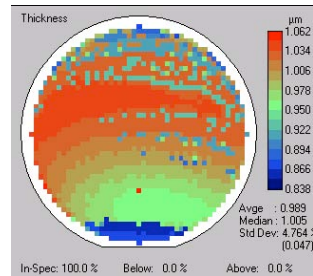
Support: NSF CTS 0219200 (ITR)

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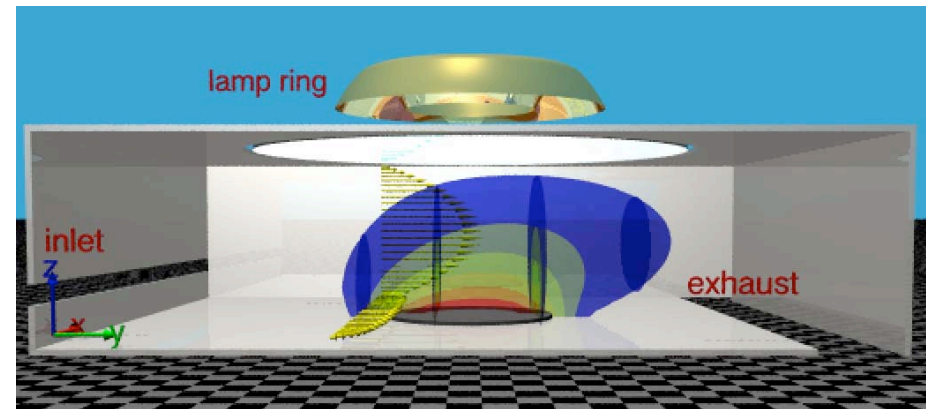




Limits of conventional CVD designs



- Inflexible
- Process throughput / uniformity trade-offs
- Few control inputs
- Limited wafer access and few sensors

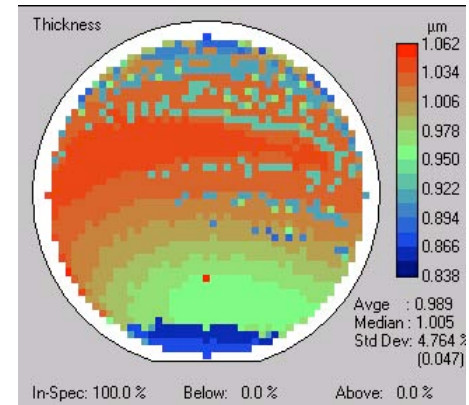
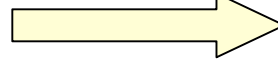




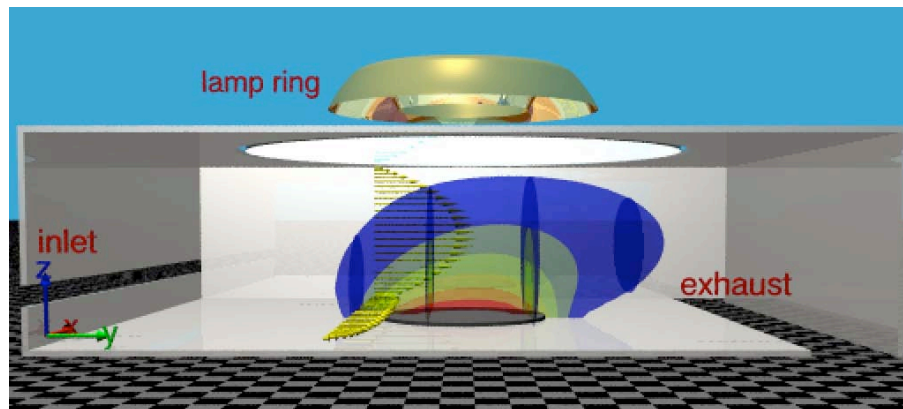
Iterative design/optimization cycle



CVD process operations leading to spatially non-uniform film growth



Simulation-based assessment of design and operation alternatives



Object-oriented CVD simulation tools for diagnosing factors responsible for non-uniformity



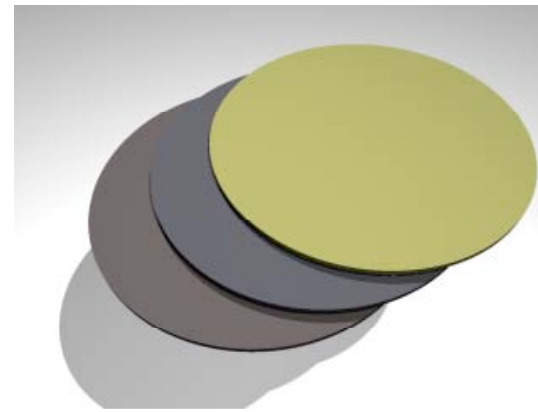
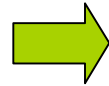


The Programmable Reactor concept

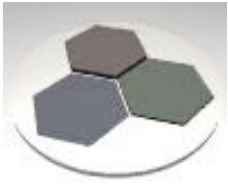
- To achieve true 2D control of reactant gas composition across the wafer surface
- To enable single wafer combinatorial experiments for process and materials discovery
- Subsequently reprogrammable for across-wafer uniformity



**Library wafer:
programmed nonuniformity**

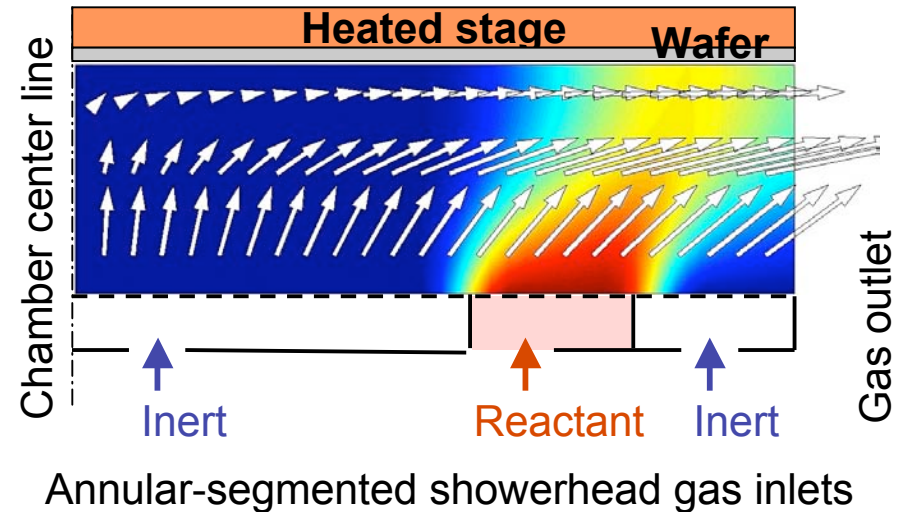


**Uniform deposition
at specified conditions**



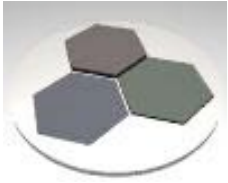
Previous efforts at gas composition control

Authors	Design innovation	Material system
Moslehi, Davis, Matthews (1995)	3 annular zone showerhead	W CVD
Van der Stricht, Moerman, Demeester, Crawley, Thru (1997)	Separate TMG, NH ₃ injection to reduce gas phase reactions	GaN MOCVD
Theodoropoulos, Mountziaris, Moffat, Han, Shadid, Thru (2000)	Annual ring showerhead with alternating TMG, NH ₃ inlet rings	GaN MOCVD
Wang, Wang, Mahanty, Komatsu, Inaoka, Nishino, Sakai (2000)	Stacked gas delivery system with inert flow forcing reactants to wafer	GaN MOCVD

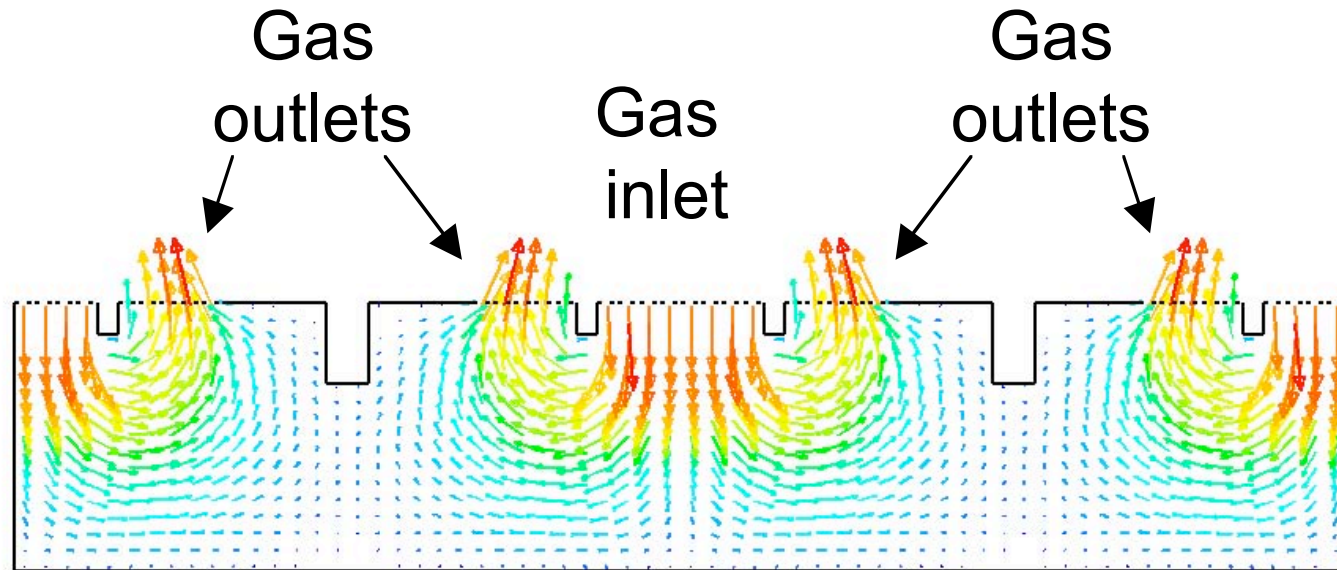


- Designs above exhaust in “conventional” ways
- Segmented designs are subject to considerable inter-segment convective transport



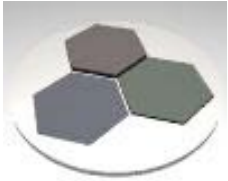


Recirculating showerhead design

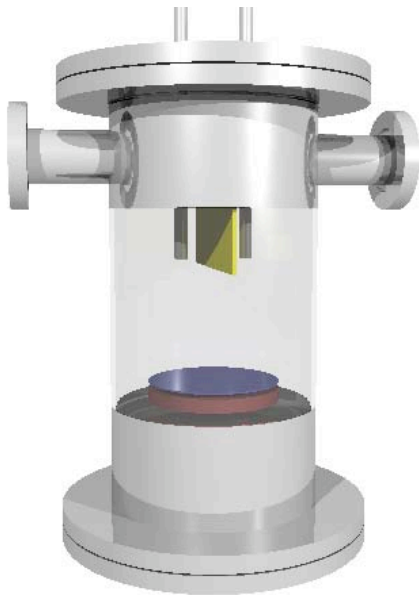


- Residual gas drawn back up through showerhead
- Periodic gas flow fields minimize inter-segment convective transport
- Residual gas can be sampled from each segment, simplifying spatial composition measurements

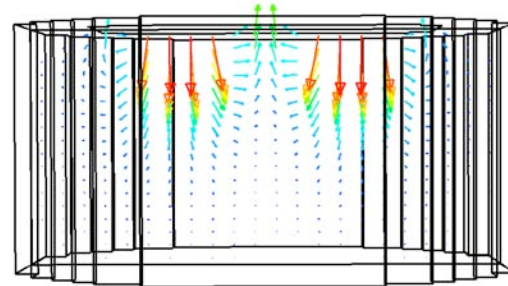




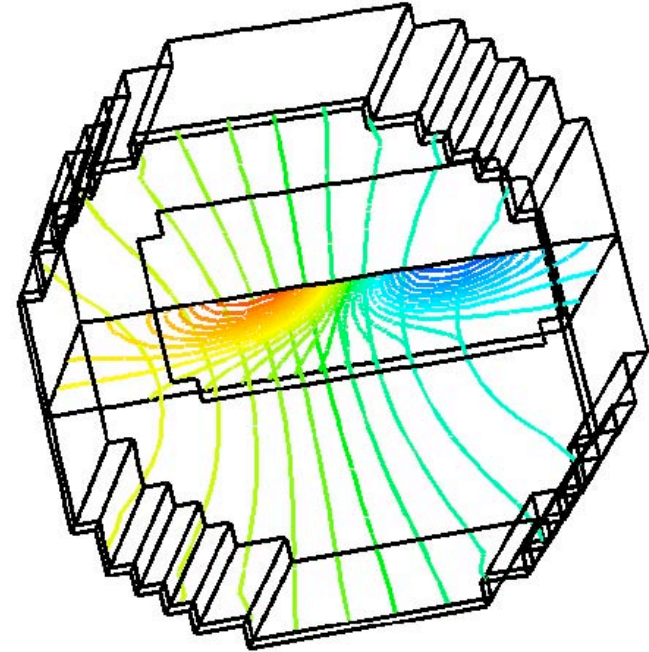
Control of gas composition gradients



2 feed/exhaust segments

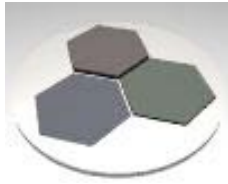


wafer plane



- Inter-segment region mass transfer is governed by diffusion
- Composition gradients are controlled by
 1. Feed composition to each segment
 2. Showerhead/wafer spacing





Design of the 3-zone prototype

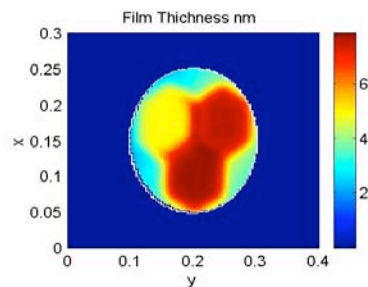
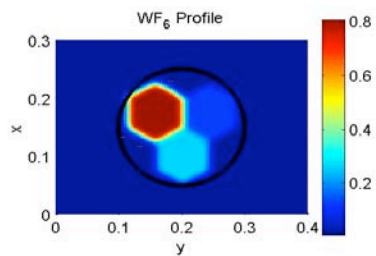
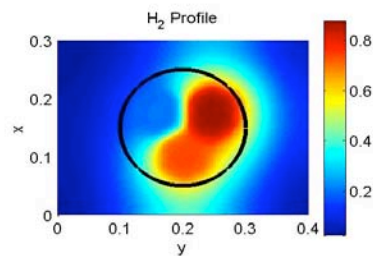
Test System:
 H_2 reduction of WF_6

Wafer temp : 673 K
Deposition time : 20 min
Flow : 60 sccm/segment

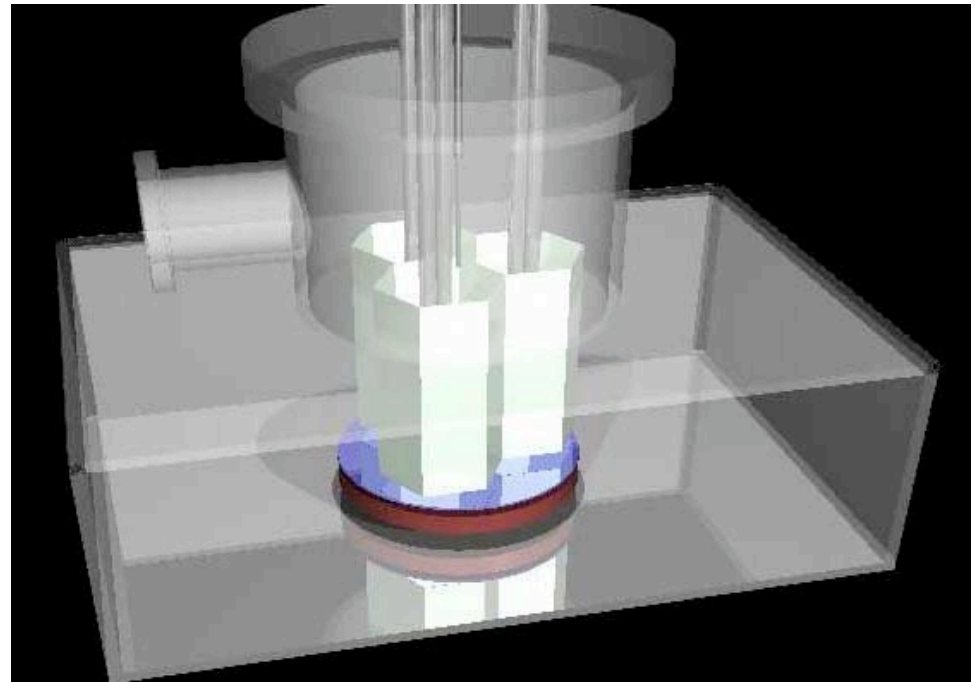
Segment 1: $x_{H_2} = 0$ $x_{WF_6} = 1$

Segment 2: $x_{H_2} = 0.8$ $x_{WF_6} = 0.2$

Segment 3: $x_{H_2} = 1$ $x_{WF_6} = 0$

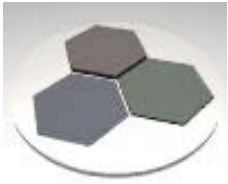


Early simulation of 2D diffusive transport in gap region for W CVD

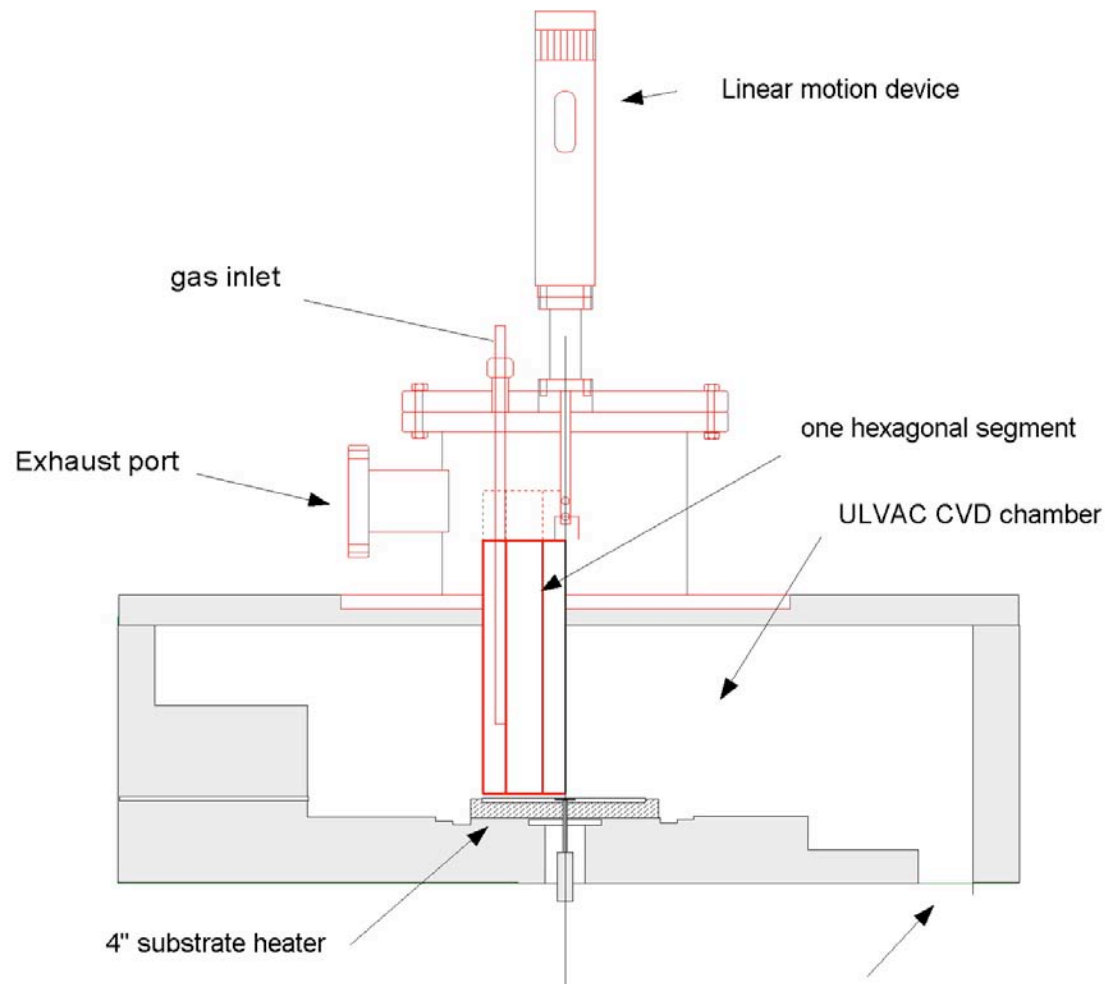


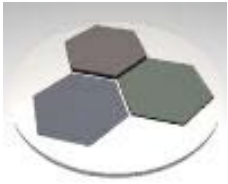
ULVAC vacuum chamber
modified for 3-segment prototype





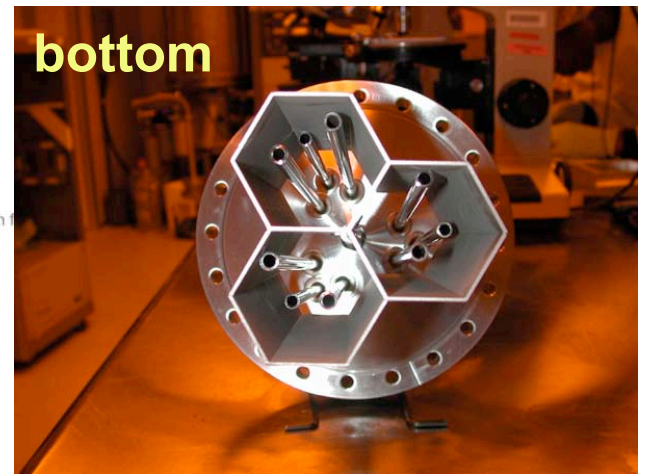
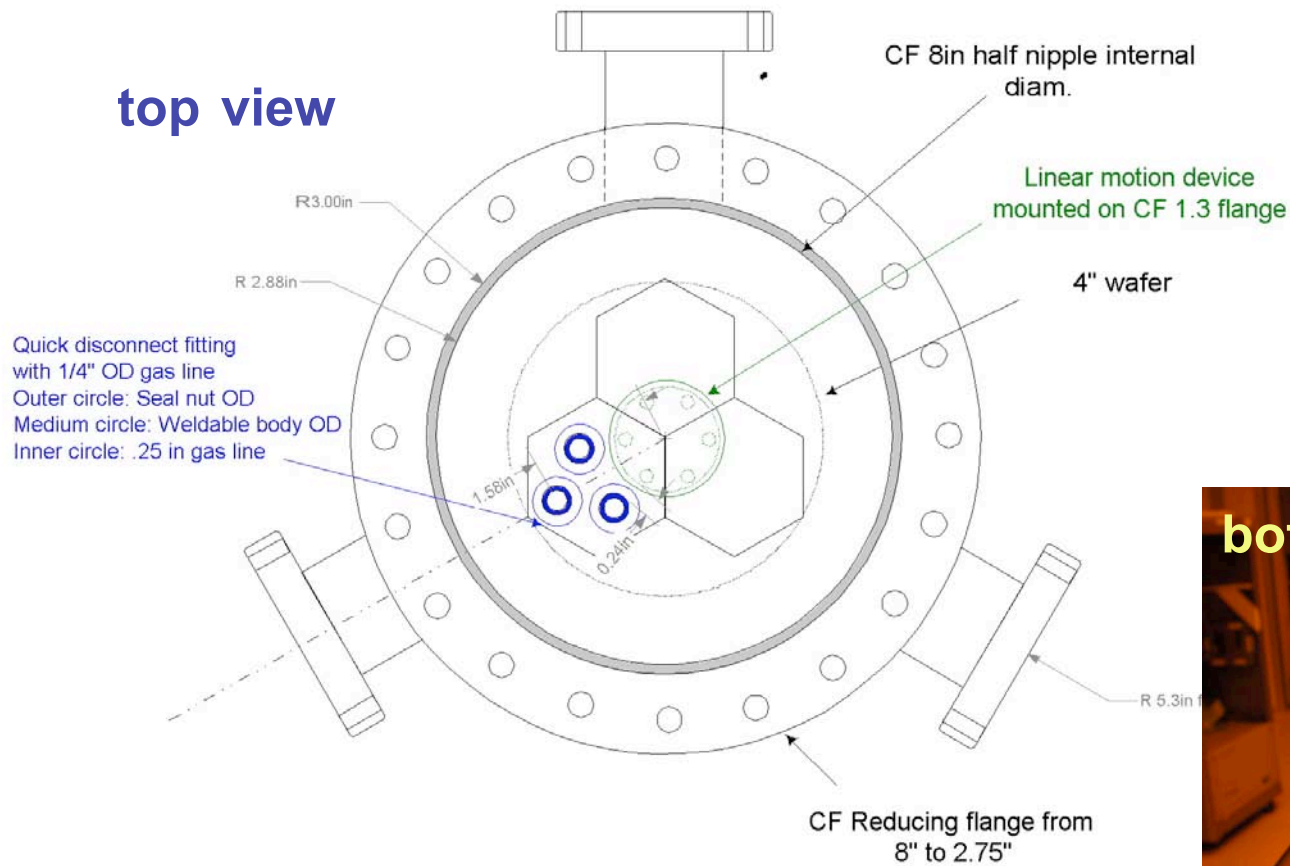
Prototype construction

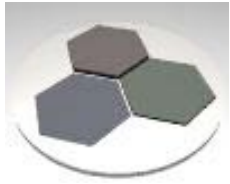




Prototype construction

top view

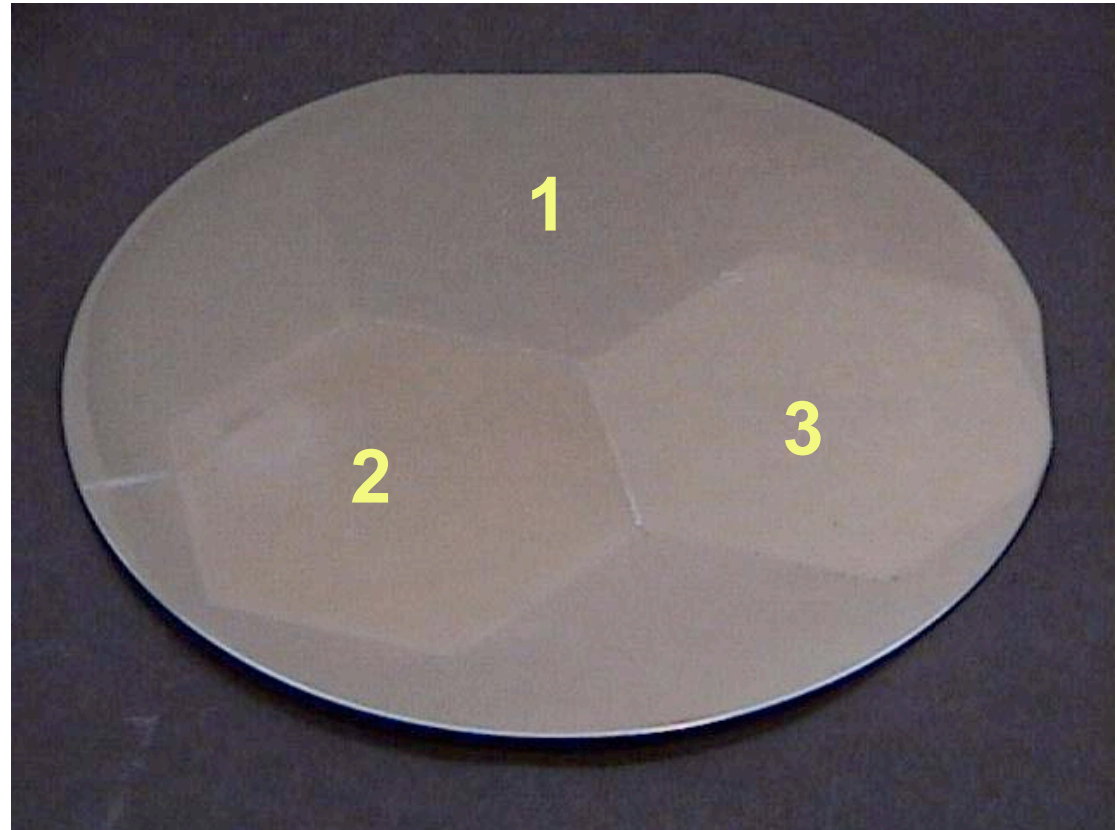




Initial experimental testing

- 3-zone prototype has been running since summer 2002
- First films deposited have demonstrated that spatially patterned wafers can be produced by controlling gas phase composition

Seg 1	50 sccm Ar
Seg 2	50 sccm WF_6
Seg 3	50 sccm H_2
0.5 torr	300-350 C



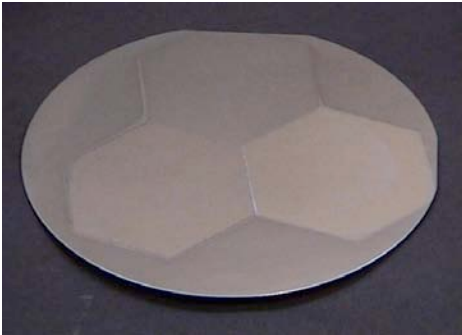
Question: Why does W deposition occur in segments 1 (Ar) and 3 (H_2)?





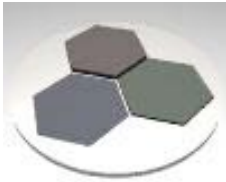
Experimental data hierarchical structure

Wafer number: w100102-03

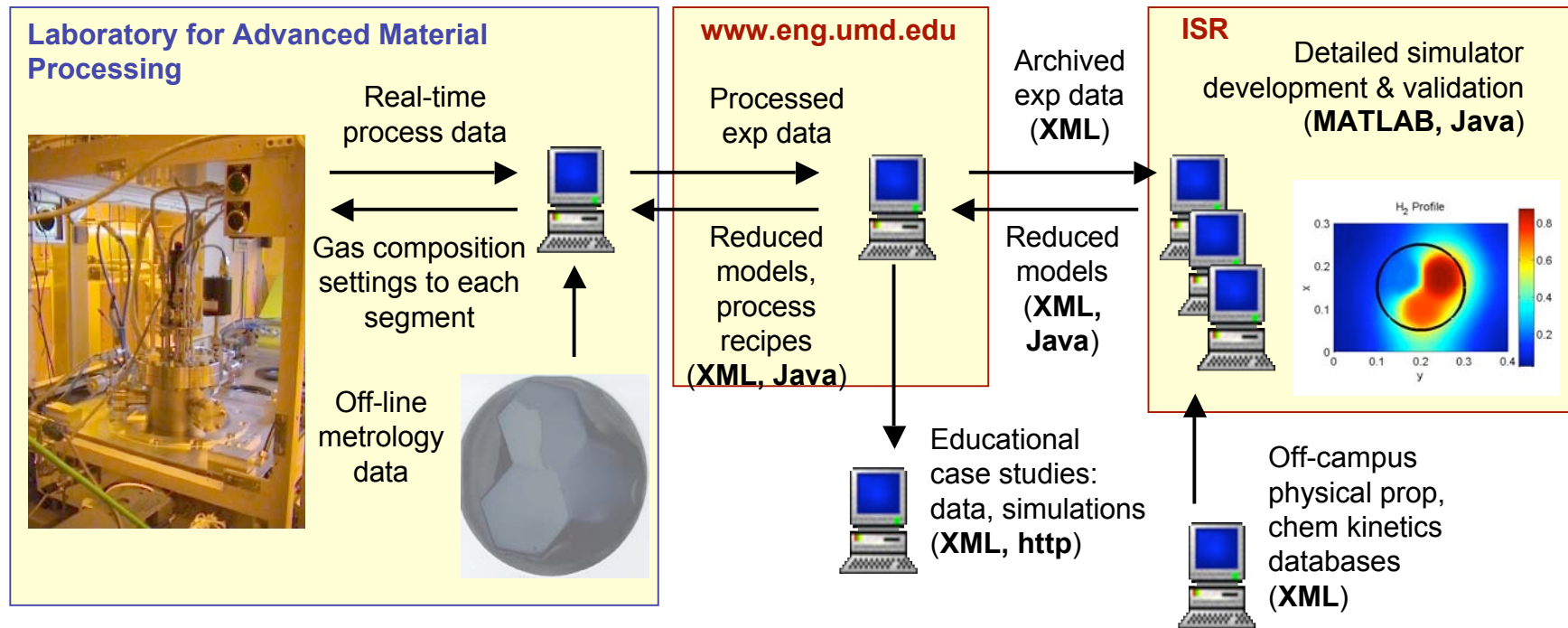


- **EquipmentData** (*process diagnosis*)
 - Gas line pressure
 - Wafer position
 - **OperatingConditions data** (*simulator input*)
 - Wafer/segment spacing
 - Segment gas flows
 - **Measurements data** (*analysis, simulator validation*)
 - Initial wafer mass
 - Final wafer mass
 - Sheet resistance profiles
- **Structure influenced by use**
- **Store raw data only**



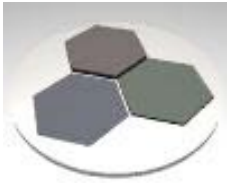


IT and distributed simulation framework



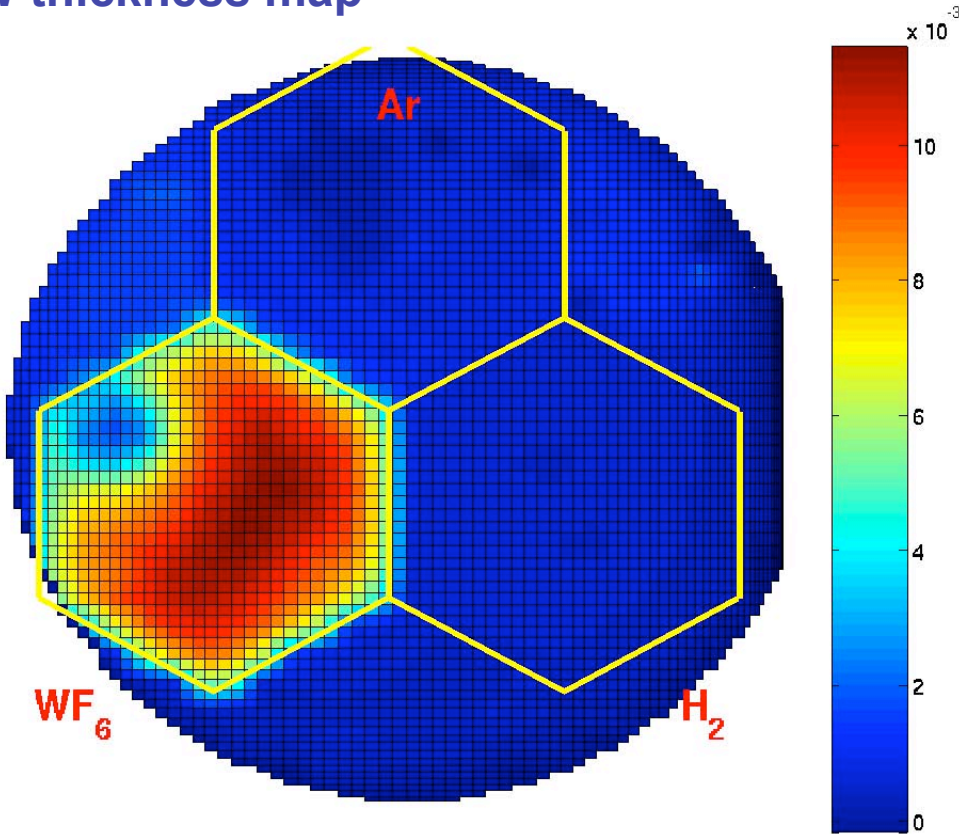
1. Represent data in XML
2. Java parser methods called from MATLAB applications





4-point probe data analysis

W thickness map

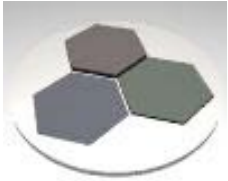


```
- <Wafer number="w091202-06">  
+ <EquipmentData>  
+ <OperatingConditions>  
- <Measurements>  
  <Current unit="A">0.001</Current>  
- <Voltage unit="mV">  
  - <Segment1R>  
    <Point11 x="1" y="1">5.90</Point11>  
    <Point12 x="2" y="1">6.91</Point12>  
    <Point13 x="1" y="3">6.01</Point13>  
    <Point14 x="2" y="3">4.70</Point14>  
    <Point15 x="3" y="3">5.68</Point15>
```

Observations

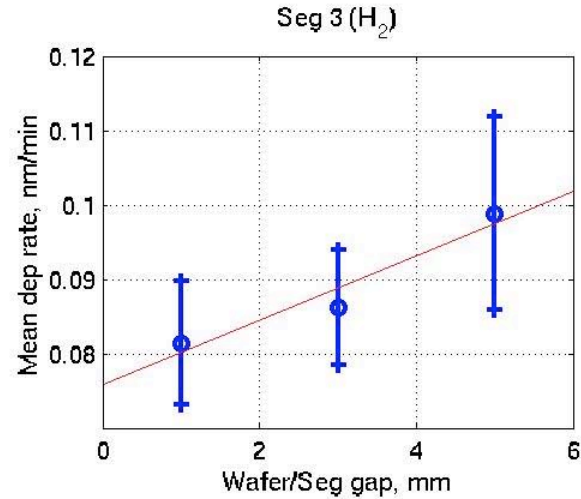
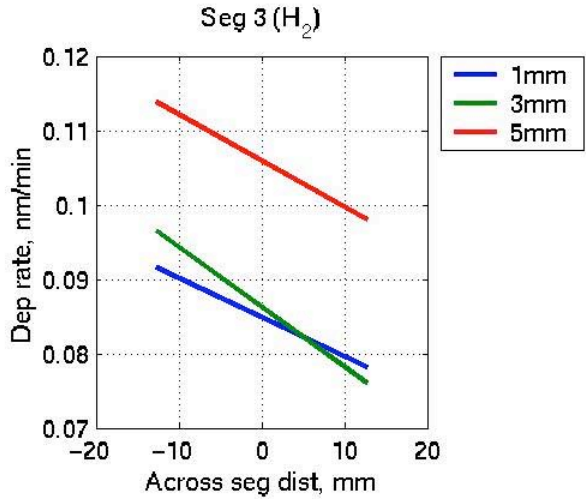
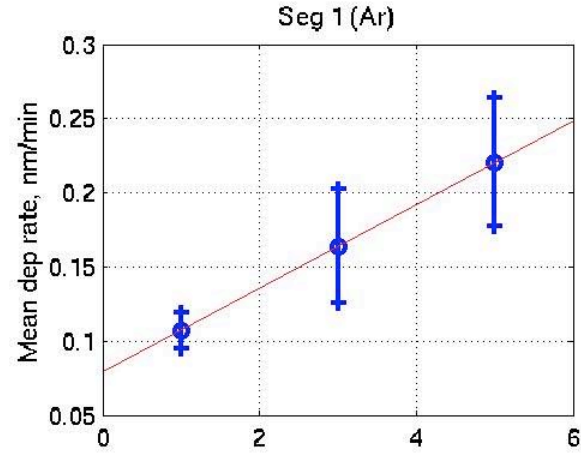
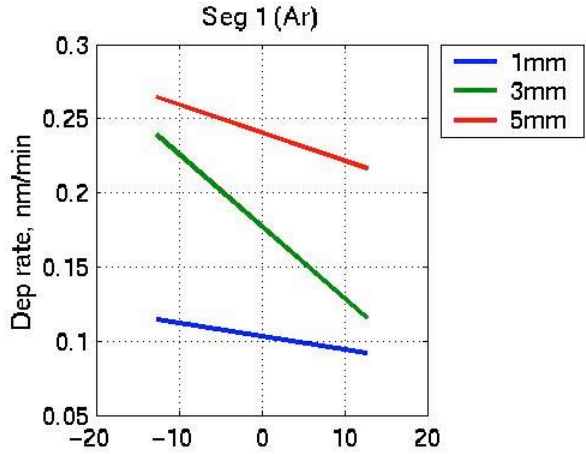
- Metrology data confirms existence of W films in Ar and H₂ segments
- Negative thickness gradient with respect to distance from WF₆ segment
- Thickness in Ar and H₂ segments grows with gap





W deposition profiles

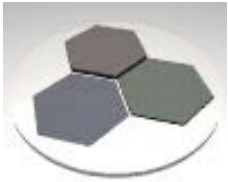
Deposition Rate



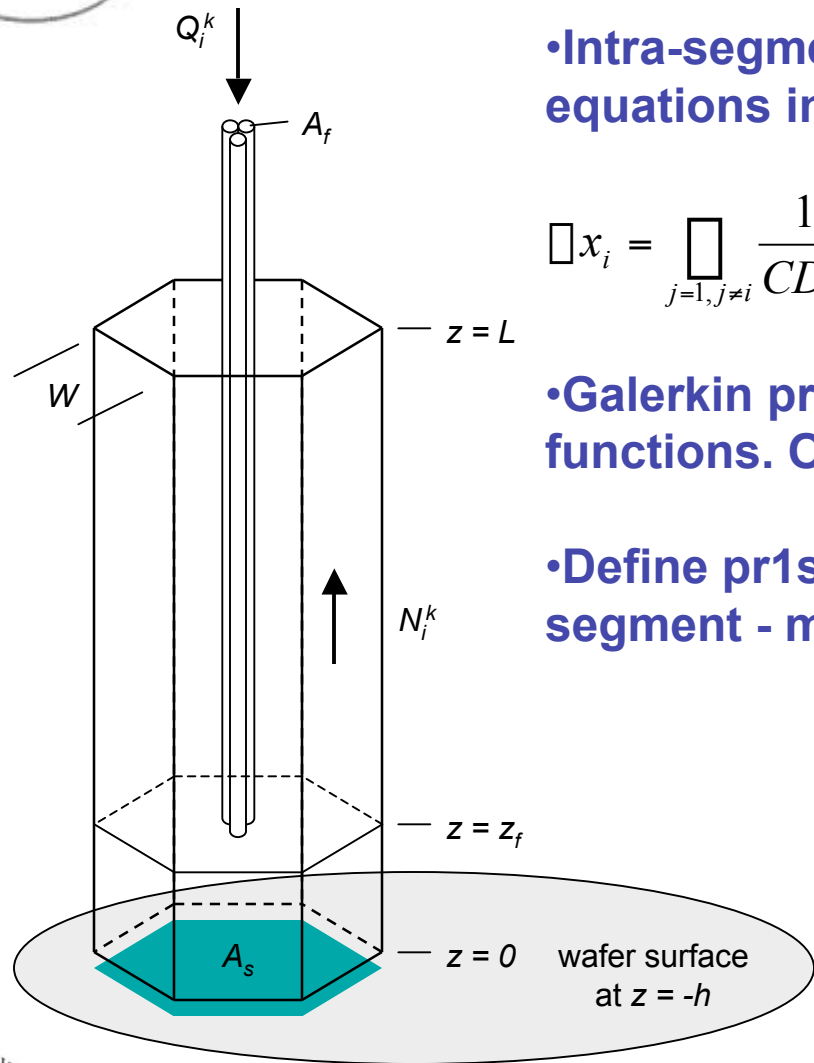
Dist from WF₆ Seg

Gap size





Segment transport model



- Intra-segment transport model: Stefan-Maxwell equations including thermal diffusion;

$$\nabla x_i = \sum_{j=1, j \neq i} \frac{1}{CD_{ij}} (x_i \bar{N}_j - x_j \bar{N}_i) \quad \bar{N}_i = N_i + \frac{\mathbf{D}_i^T}{M_i} \nabla \ln T$$

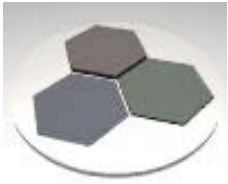
- Galerkin projection solution on global basis functions. Outlet BC: exhaust volume model;

- Define pr1seg class objects to model each segment - modularity;

- Define wafer/showerhead gap region inter-segment diffusion model object;

- Download operating conditions from data archive website to define objects.





Object-oriented MWR

Benefits to hiding details of computations:

1) Clear connection between modeling equations and solution procedure

2) One-to-one correspondence between computational tools and steps to implement MWR

Model

$$\frac{\partial T}{\partial t} = \nabla^2 T - v_x \frac{\partial T}{\partial x} + R_c(T)$$

$$T(x, y, t) = \sum_{i=1}^M \sum_{j=1}^N a_{i,j}(t) \phi_i(x) \psi_j(y)$$

$$\text{F.val} : \{ \phi, \psi \}$$

$$\text{F.dir} : [1, 2]$$

$$\text{F.wt} : \{ \mathbf{w}_x, \mathbf{w}_y \}$$

Basis function object

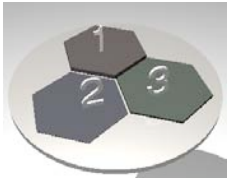
Overloaded operators and functions

$$\mathbf{T} = \mathbf{a} * \mathbf{F}$$

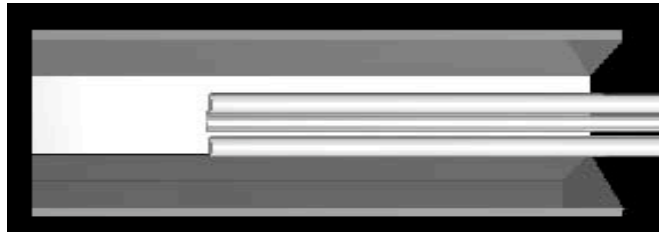
$$\dot{\mathbf{a}} = \text{wip}(\text{DDX} * \mathbf{T} + \text{DDY} * \mathbf{T} - \mathbf{v}_x * \text{DX} * \mathbf{T} + \mathbf{R}_c, \mathbf{F})$$

Adomaitis, Comp & ChE, 2002

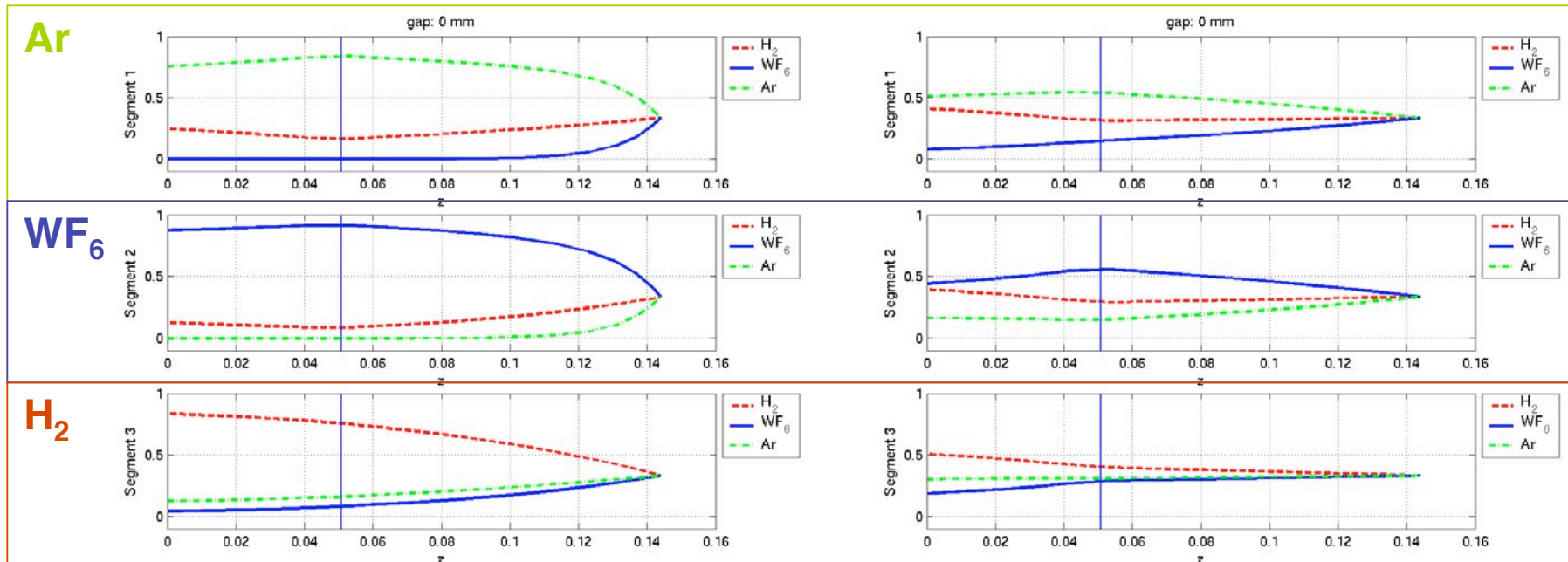




Segment gas composition profiles



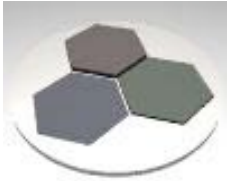
- Close wafer/showerhead spacing
- Significant effect of feed gas flow
- Thermal diffusion effects
- Back-diffusion from common exhaust region to wafer surface



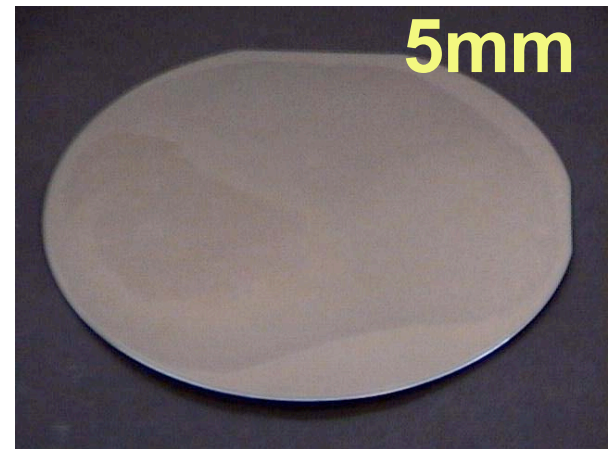
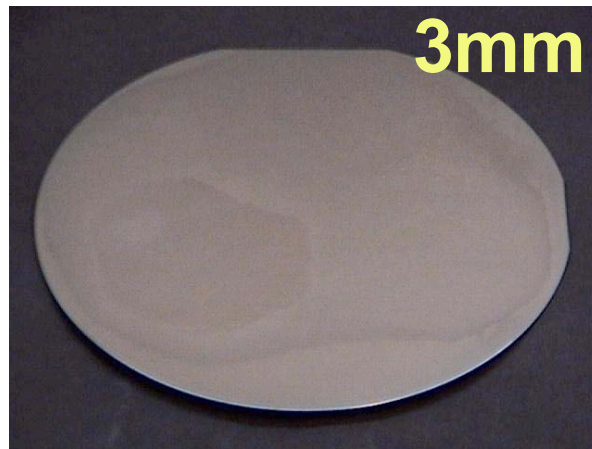
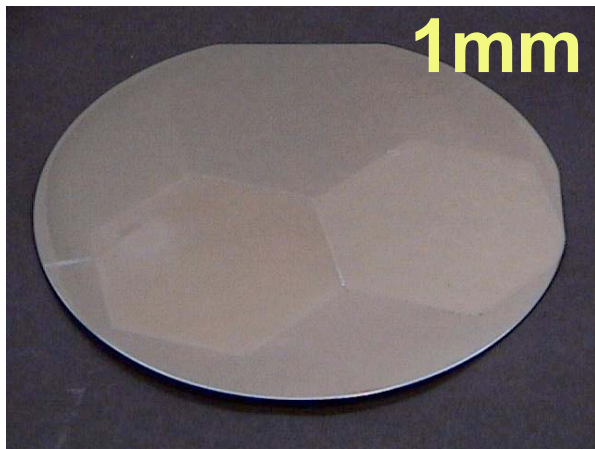
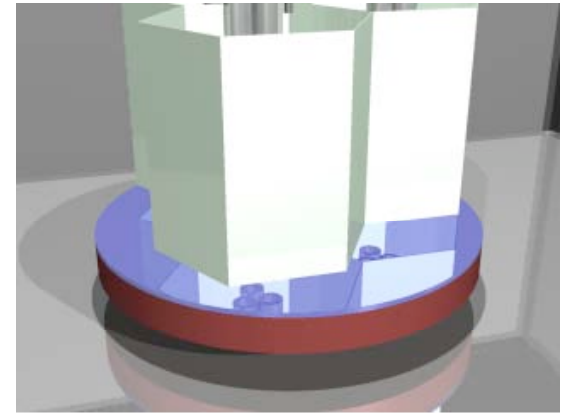
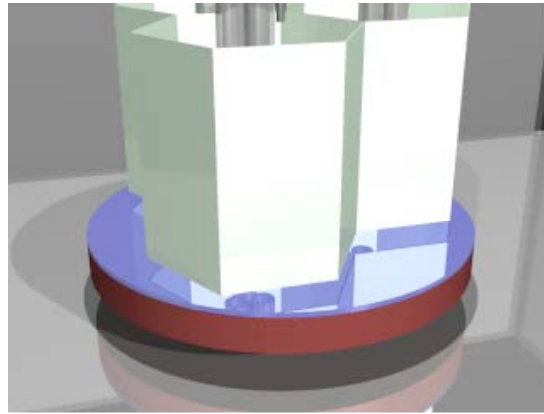
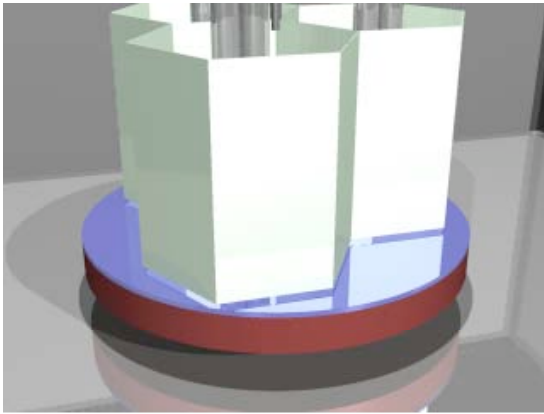
50 sccm / segment

5 sccm / segment





Deposition pattern control



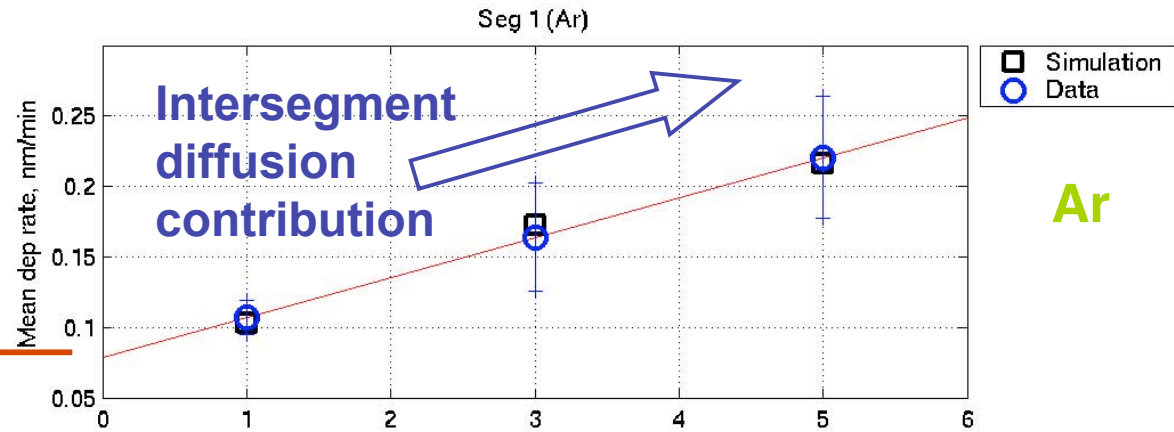
Increasing across-wafer diffusion



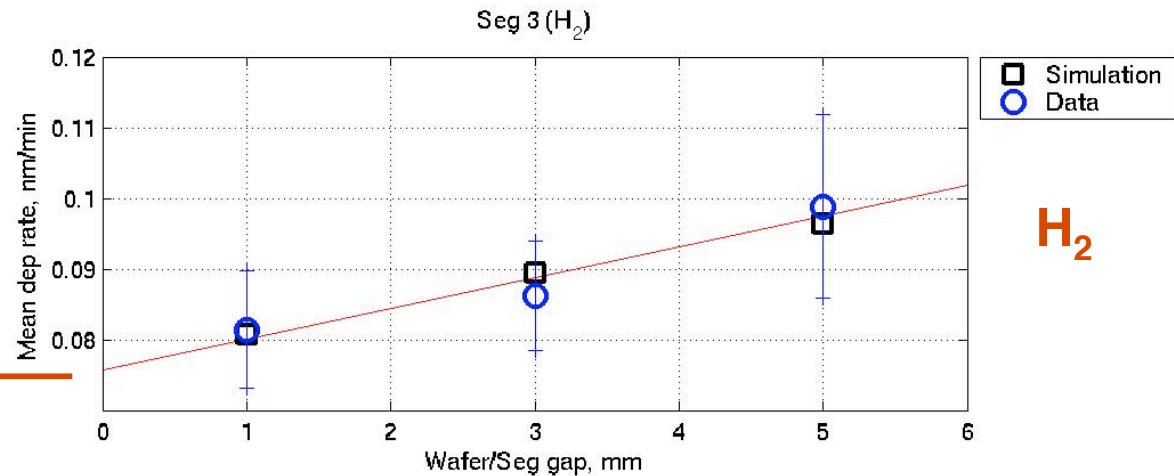


Effect of gap size on film thickness

Back diffusion contribution

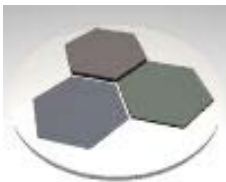


Back diffusion contribution

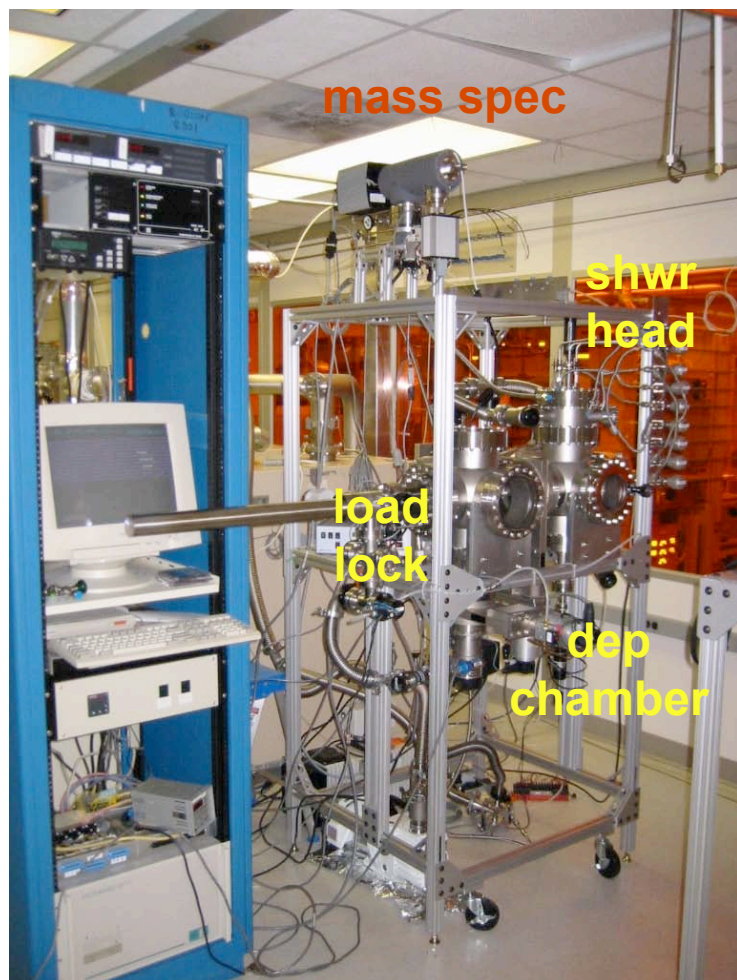


Gap size





Current Programmable Reactor research



- Complete reconstruction of 3-zone prototype to improve reliability and achieve true programmability;
- Simulation-based design of next generation reactor: more segments per showerhead; smaller segments incorporating micro-fabricated flow control; improved manufacturability.





Conclusions

- A new approach to spatially controllable CVD was presented; reactor featured a reverse-flow, segmented showerhead design;
- Gas composition to each segment can be controlled and sampled;
- Gas composition at wafer surface is governed intra-segment back diffusion (controlled by gas feed rate) and across wafer inter-segment diffusion (controlled by wafer/showerhead gap size);
- 3 zone prototype was constructed; initial testing demonstrated the feasibility of spatial patterning in CVD;
- Major overhaul of prototype is complete;
- Extensive use of simulation tools for reactor design and interpretation of experimental data

